Inerting a B-747 SP Center Wing Fuel Tank Scale Model with Nitrogen Enriched Air



William M. Cavage FAA Fire and Cabin Safety Conference October 22-25, 2001 Atlantic City, NJ

Outline

- Background
- Model
- Instrumentation
- NEA Distribution
- Equations
- Test Data
- Summary

Background

- FAA is Seeking to Improve Upon Existing Fuel Tank Safety in Fleet in the Wake of TWA800 Air Disaster
- Inerting of Fuel Tanks Could Provide Significant Fuel Tank Protection. Most Available Data on Fuel Tank Inerting for Rectangular Box
- Focus of the Testing is to Validate Existing Assumptions for Inerting Complex Geometric Spaces (Commercial Transport Fuel Tanks) as Compared to Simple Rectangular Boxes
- Also, Use Model to Determine the Most Efficient Deposit Configuration

Description of Model

- Quarter-Scale Model of Boeing 747 SP CWT was Built from Three Quarter Inch Plywood By Scaling Drawings from Shepherd Report
 - 24% length Scale (1.2% Volume)
- Spars and Spanwise Beams Simulated with Quarter Inch Plywood Installed in Slats with Scaled Penetration Holes
- Vent System Simulated with PVC Tubing Plumbed to an Aluminum Vent Channel Adhered to a Plywood Top
- Removable Lid to Allow for Model Maintenance and Modification

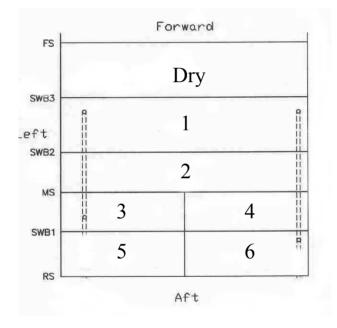
Photo of Model



Instrumentation

- Oxygen Sensor in Each Bay and in One Vent Channel
 - Sample Returned to Each Bay to Have Minimal Effect on Inerting Process
 - Sensors Plumbed in Unique Sample "Drafting" Method
 - Sensor Remote From Analyzer
- Thermocouple in Each Bay to Detect Temperature Changes During Testing
- NEA Generator Equipped with Oxygen Analyzer
 - Calibrated and Checked before Each Test
 - Used to Calibrate all Other Sensors

B-747 SP Bay Diagram with Volume Data



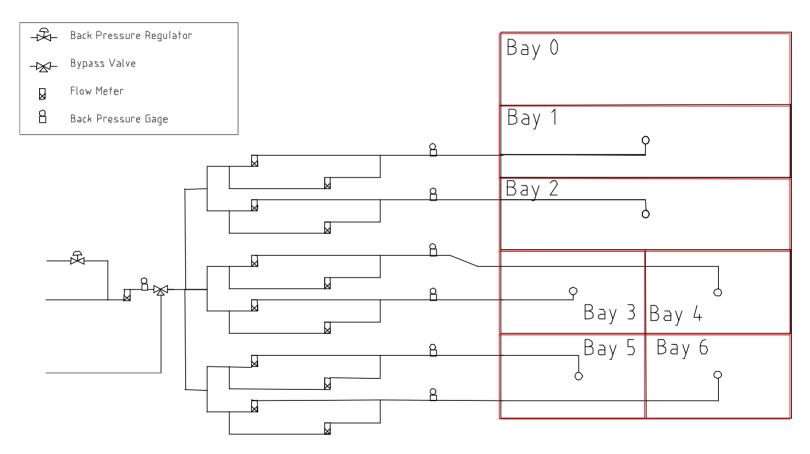
| Bay | Calculated Volume | Scaled Value | Percentage of Tank | Sheppard Volume | Percentage Volume |
|--------|----------------------|-----------------|-----------------------|--------------------|----------------------|
| 0(dry) | 546.1 | 7.549 | n/a | 536.7 | n/a |
| 1 | 577.7 | 7.986 | | 543.9 | |
| 2 3 | 421.1 188.2 | 5.823 2.602 | | 392.0 196.0 | |
| 4 5 | 188.2 239.6 | 2.602 3.312 | | 196.0 220.7 | |
| 6 | 239.6 | 3.312 | | 220.7 | 12.5% |
| Total | 1854.4 | 25.637 | 100% | 1769.3 | 100% |

Reported Volume = 1775Percent Difference = 4.47 %

NEA Distribution System

- "Variable Manifold" Allows for Depositing NEA in Any and All Bays of the Tank at Different Flow Rates
 - Accepts Output of NEA Generator and is Plumbed to a Bank of Flow Meters
 - Two Flow Meters in Parallel for Each Bay to Allow for Both Large and Small Deposit Quantities
 - Measure Meter Back Pressure for Accurate Flow Reading
- Used Directing Nozzles on NEA Deposit Fittings for Some Uneven Deposit Cases

NEA Distribution System Diagram



Equations Used

Volumetric Tank Exchange (VTE)

Volumetric Tank Exchange =

Time * Volume Flow Rate Fuel Tank Volume

Weighted Volumetric Average

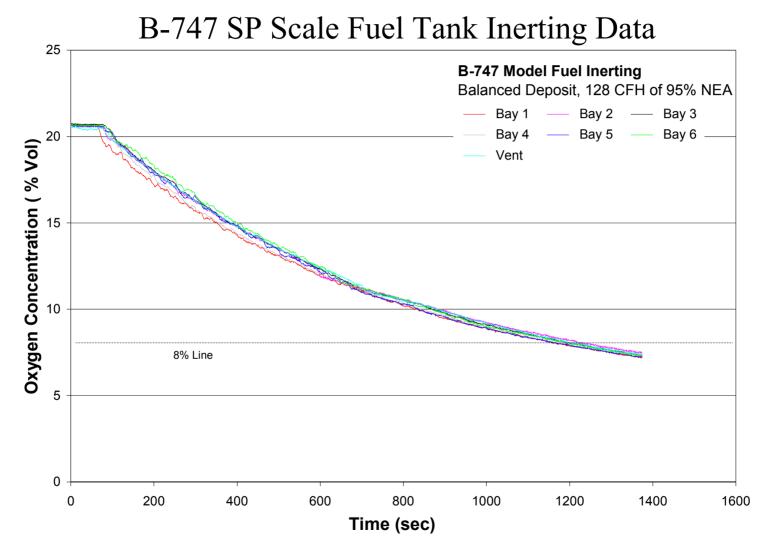
 $Volumetric \ Average = \frac{7.986[O_2 \ Bay1] + 5.823[O_2 \ Bay2] + 2.602[O_2 \ Bay3] + 2.602[O_2 \ Bay4] + 3.312[O_2 \ Bay5] + 3.312[O_2 \ Bay6]}{25.637}$

Inerting Solution (Perfect Mixing) $O_2(t) = O_{2_{Amb}} - [(O_{2_{Amb}} - O_{2_{NEA}})(1 - e^{-VTE})]$

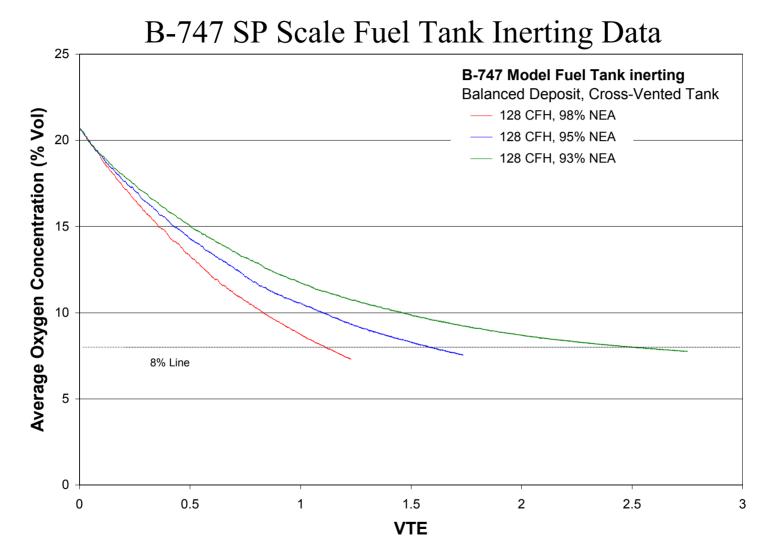
Empirical Solution (FAA Ullage Washing Data) $O_2(t) = O_{2_{Amb}} - [(O_{2_{Amb}} - O_{2_{NEA}})*$ (-0.0145VTE⁴ + 0.1345VTE³ - 0.5275VTE² + 1.0873VTE - 0.0121)]

Cross-Vented Configuration Data

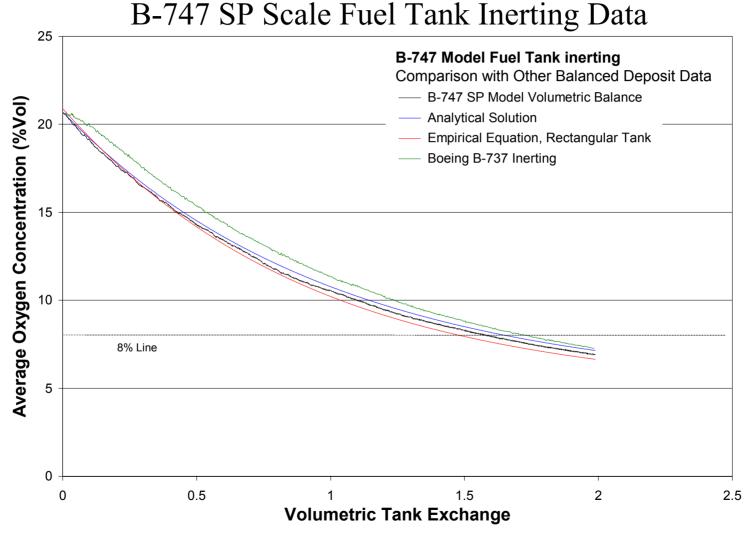
- Inerted Tank Several Times with Different NEA Oxygen Concentrations with the Goal of Balancing the Flow into Each Bay to Obtain "Equal Inerting"
- Used the Volumetric Average Developed to Make Comparisons with Other Inerting Runs
- Results As Expected and Consistent with Previous Testing but New Numbers Point Toward a VTE of 1.6 for 95% NEA
- Depositing in and Uneven Manner Can Simplify Manifold and Have No Negative Impact on the Inerting Process



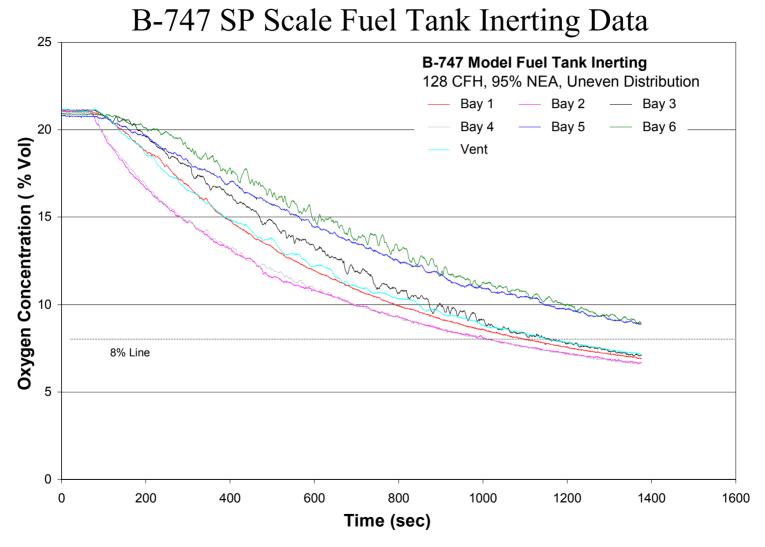
FAA Fire and Cabin Safety Conference



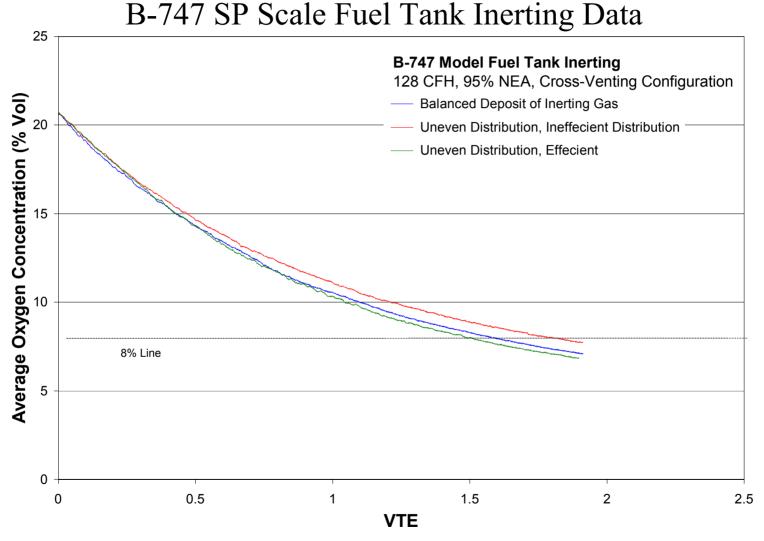
FAA Fire and Cabin Safety Conference



FAA Fire and Cabin Safety Conference



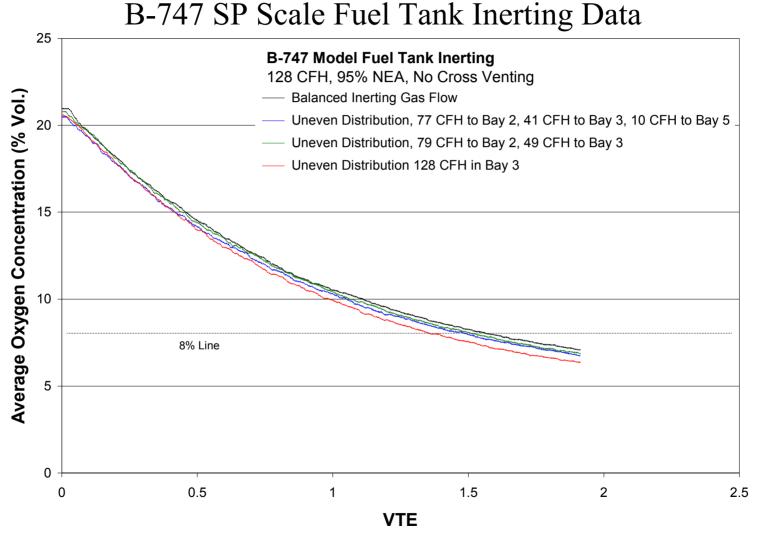
FAA Fire and Cabin Safety Conference



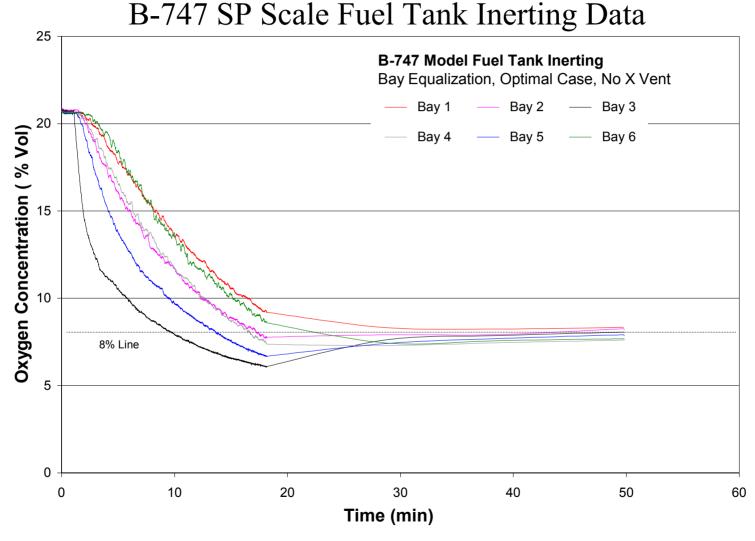
FAA Fire and Cabin Safety Conference

Blocked Vent Configuration Data

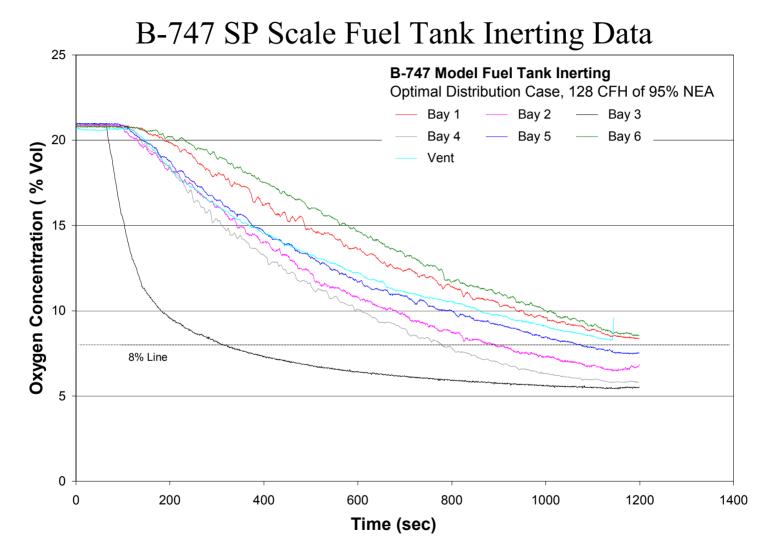
- Inerted Tank Several Times with NEA 95% to Minimizing the NEA Volume Required to Inert the Tank with Left Half of Vent System Blocked (No Cross Venting)
 - First did Balanced Run to Give Baseline; Used the Volumetric
 Average Developed to Make Fair Comparisons with Other Methods
- Results Illustrated Modest Improvement with Simplest
 Deposit Scheme
 - Deposit Scheme Has Poorer NEA Distribution But Data Indicates
 Oxygen Concentration From Bay to Bay Will Diffuse
 - Method Does Not Appear to Be Sensitive to Flow Rate and NEA %
- Comparisons with Full-Scale Data Marginal, VTE Consistent



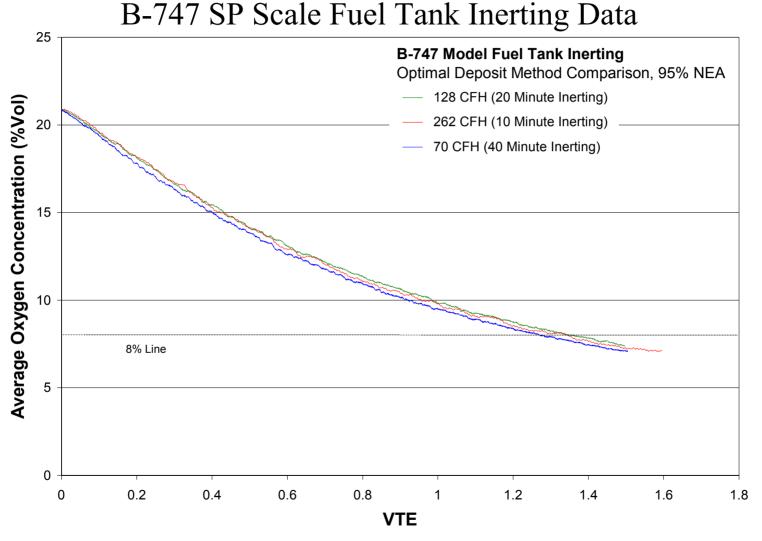
FAA Fire and Cabin Safety Conference



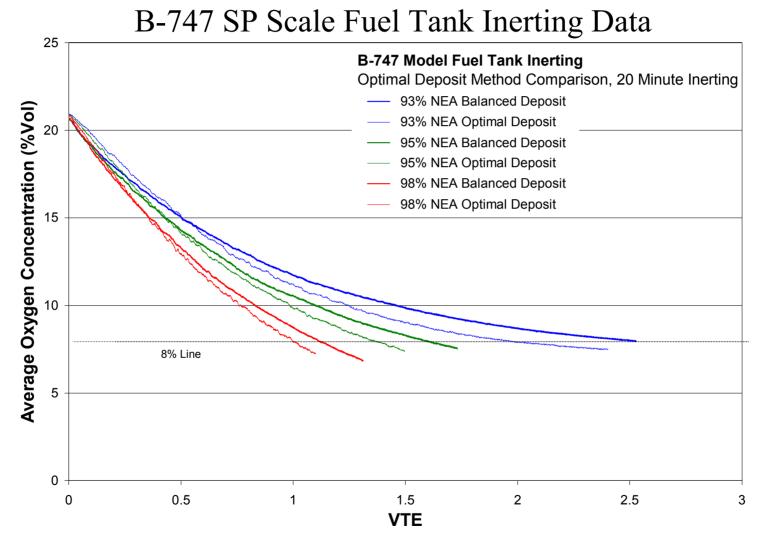
FAA Fire and Cabin Safety Conference



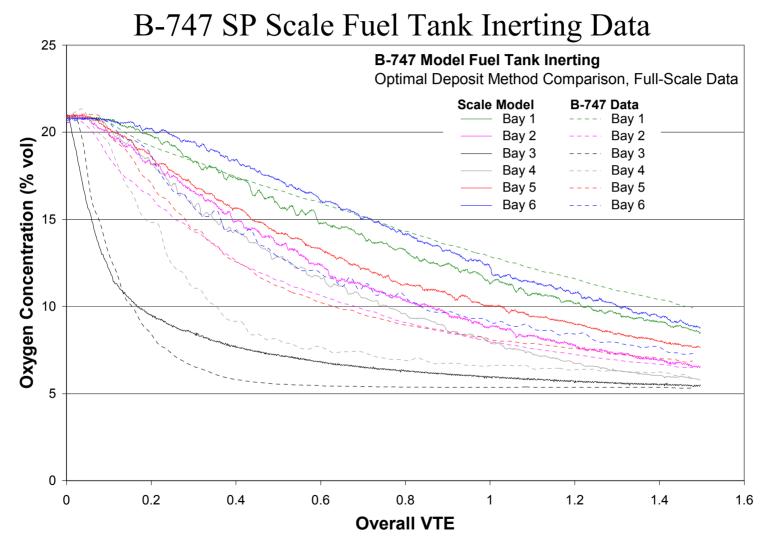
FAA Fire and Cabin Safety Conference



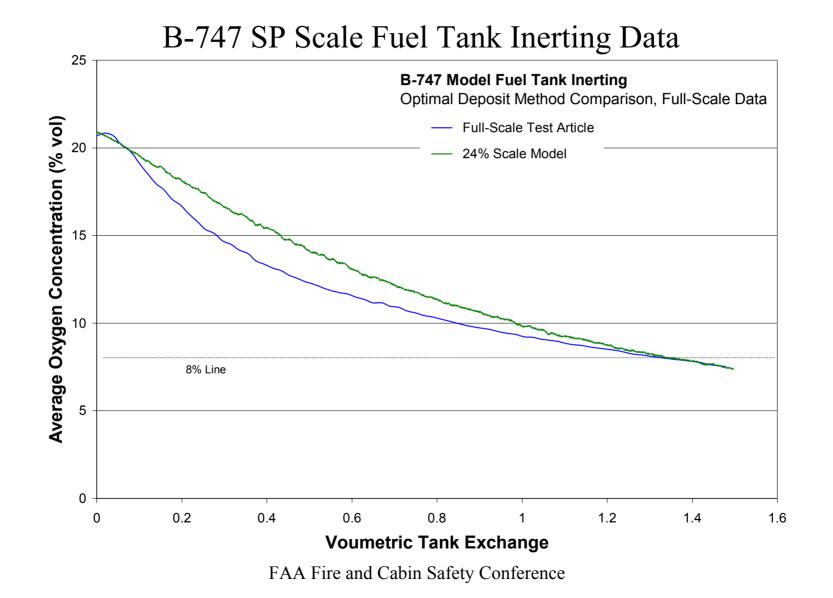
FAA Fire and Cabin Safety Conference



FAA Fire and Cabin Safety Conference



FAA Fire and Cabin Safety Conference



Summary

- Model Results Consistent with Existing Knowledge Base But VTE Slightly Higher Then in Original FAA Experiments
 - This is Believed to be due to Better Measurement Techniques Developed
- Depositing in an Efficient Manner Can Greatly Simplify Manifold Design and Even Improve Inerting Efficiency
- Initial Full-Scale Test Article Data Highlight Potential Deficiencies with this Design Methodology. More Testing Needed to Verify the Limitations of Scale-Model Inerting Evaluation