



Influence of Printing Parameters on the Flammability Behaviour of 3D Printed Polyetherimide

Ninth Triennial International Aircraft Fire and Cabin Safety
Research Conference, October 30th, 2019

T. Krause, Airbus Fire Safety Engineering & Fire Test

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Agenda

- Outline
- Printing technology, materials and parameters
- Parameter variation and test procedure
- Results
- Discussion
- Summary

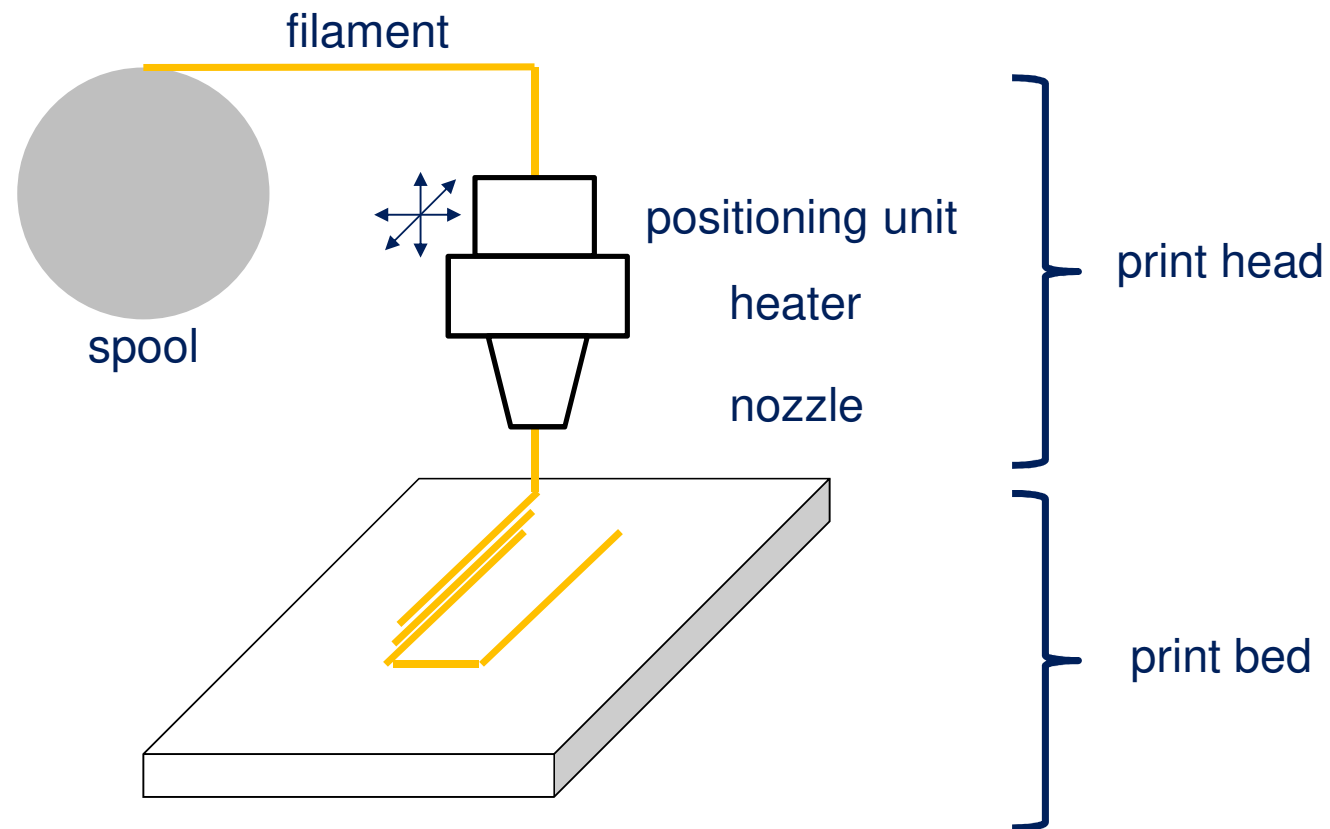
Outline

- Additive manufacturing allows for material modifications impossible with conventional production techniques. It is unclear to what extent these modifications alter the flammability behaviour
- A task group was founded at the FAA Materials Fire Test Forum in June 2018 to investigate the influence of printing parameters
- Decision to start with Fused Deposition Modelling (FDM) and Polyetherimide Ultem 9085 CG as both printers and material were available at different locations

Printing technology, materials and parameters

Fused Deposition Modelling

Printer	Fortus 450mc & 900mc by Stratasys
Location	Stratasys, Eden Prairie Airbus, Hamburg
Material	Polyetherimide ULTEM 9085 by Sabic Certified Grade filaments by Stratasys
Build	6 layers, 0.254 mm per filament → 1.5 mm thickness Always: Seam of 1 filament with full infill



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Printing technology, materials and parameters

Part design

- “Replica” of conventional part
- Bio-inspired (bone-like) complex structures

Post processing

- For the specimen: e.g. removal of support, or for the part: e.g. grinding/sanding to certain surface quality
- Spatula, fillers, topcoats

Build

- Printing directions
- Raster angle
- Layer thickness
- Thickness
- Infill (%)
- Single specimens vs. cut from bigger plate

Manufacturing technology

- Fused Filament, laser sintering, powder bed etc.
- Printer manufacturer and type
- Layer thickness
- Print speed and temperature

Material

- Material itself is a variable
- ALM type vs. standard type of same material
- Filament thickness

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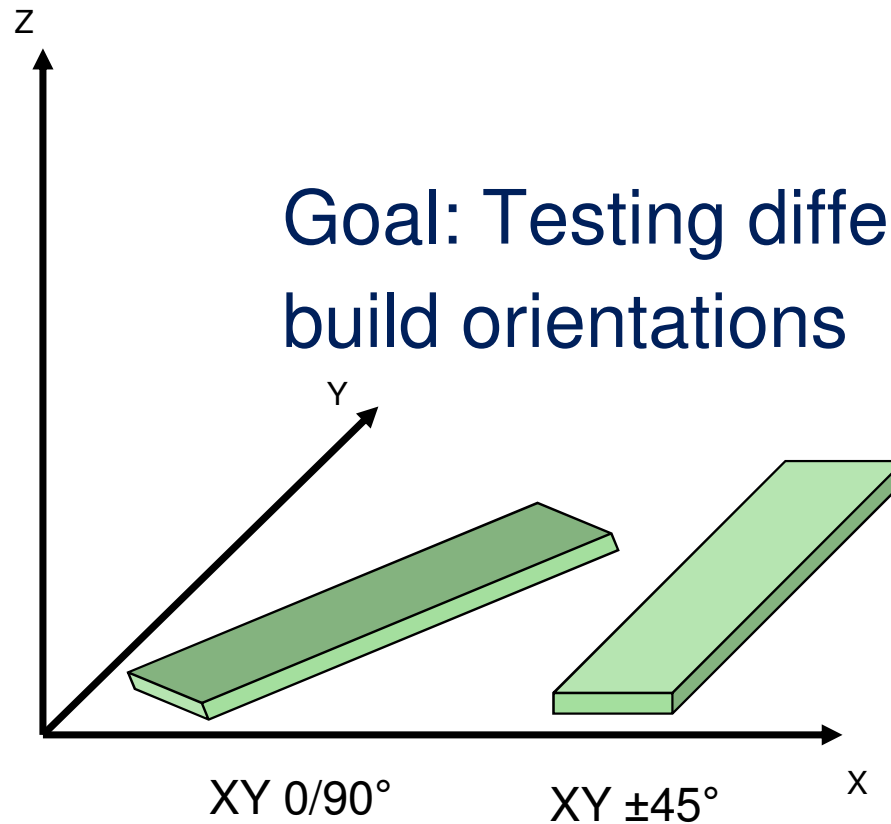
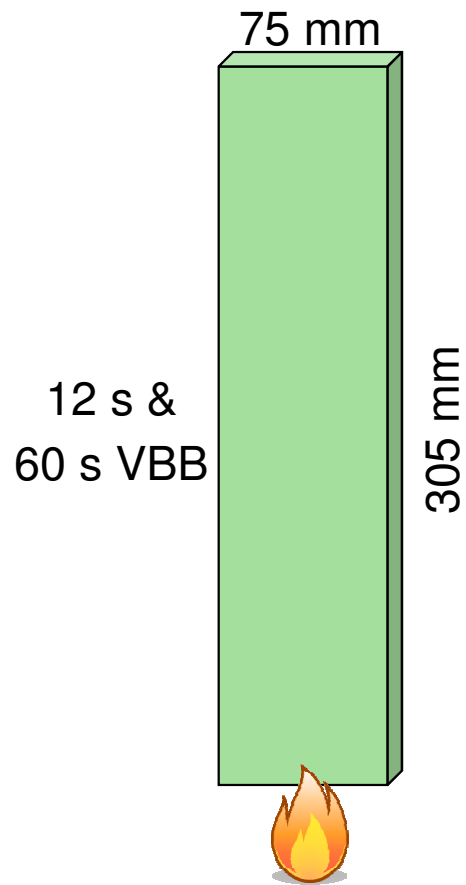
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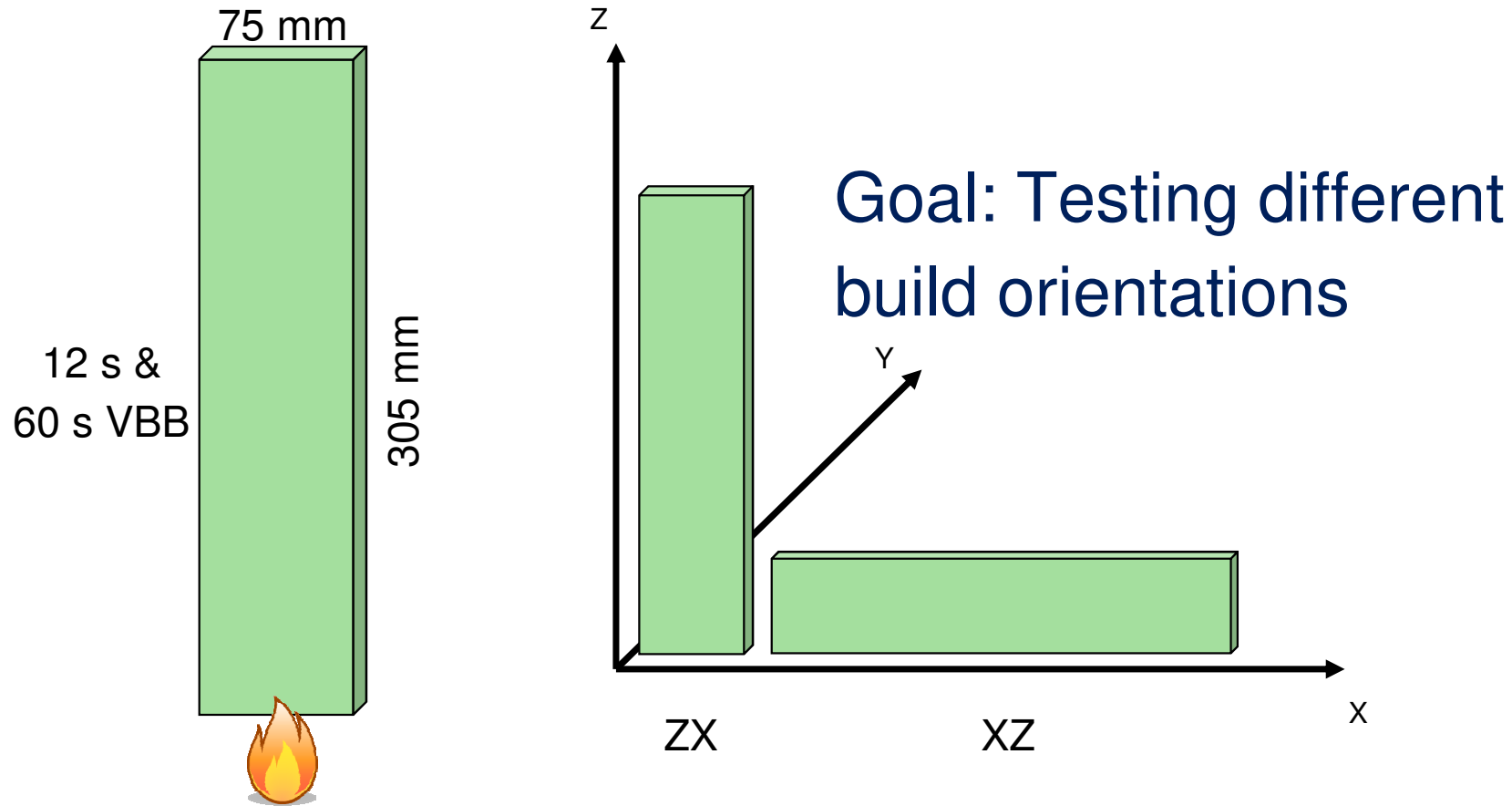
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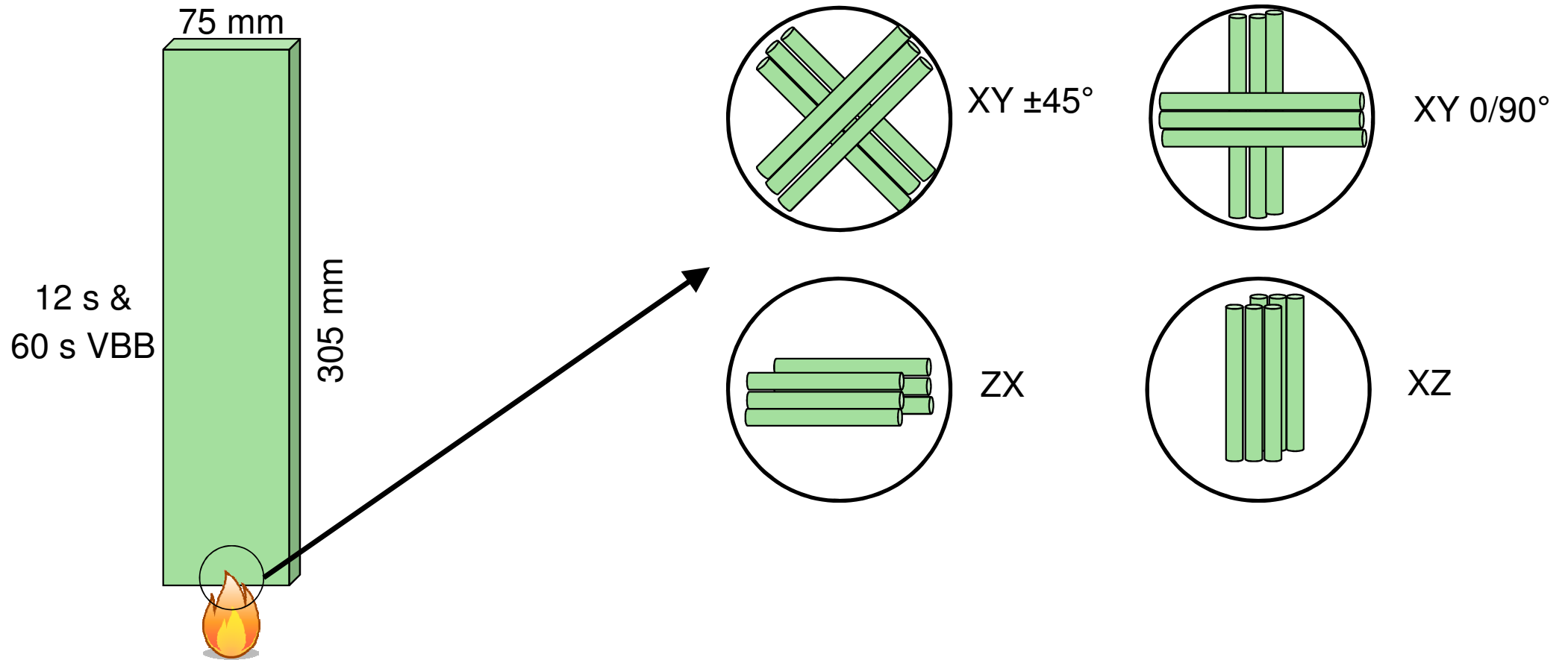
Parameter variation and test procedure: orientation



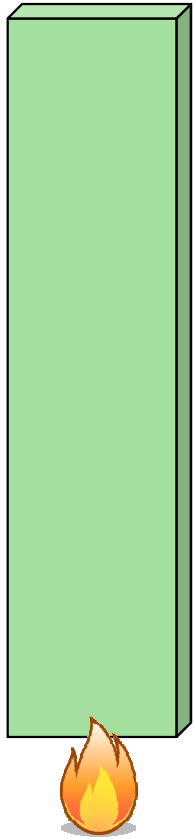
Parameter variation and test procedure: orientation



Parameter variation and test procedure: orientation



Parameter variation and test procedure: infill

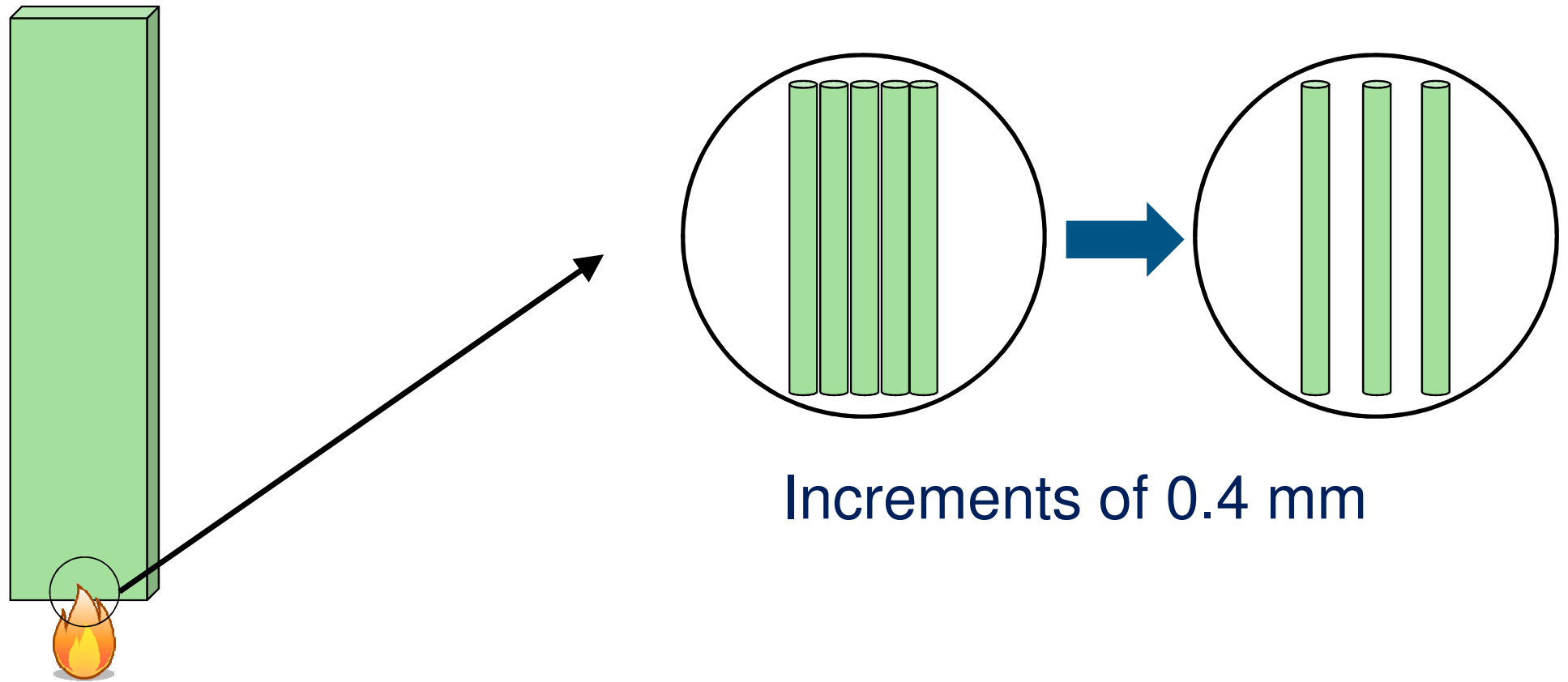


Goal: Reduce amount of material whilst maintaining the outer shape

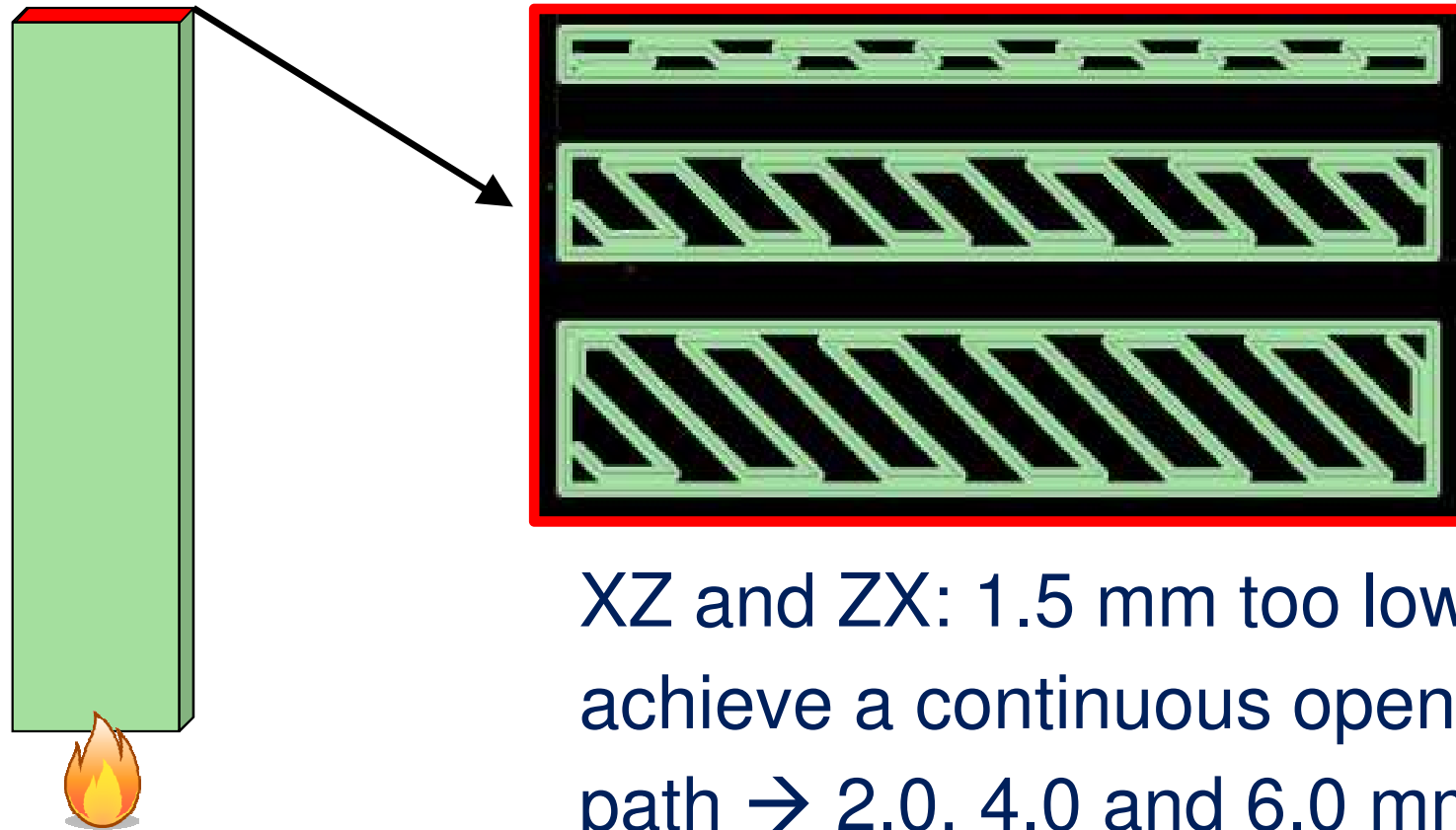
Means: Vary the distance of filaments to each other

Infill: Ratio of coupon weight vs. weight of densest packed coupon, normalised by thickness

Parameter variation and test procedure: infill

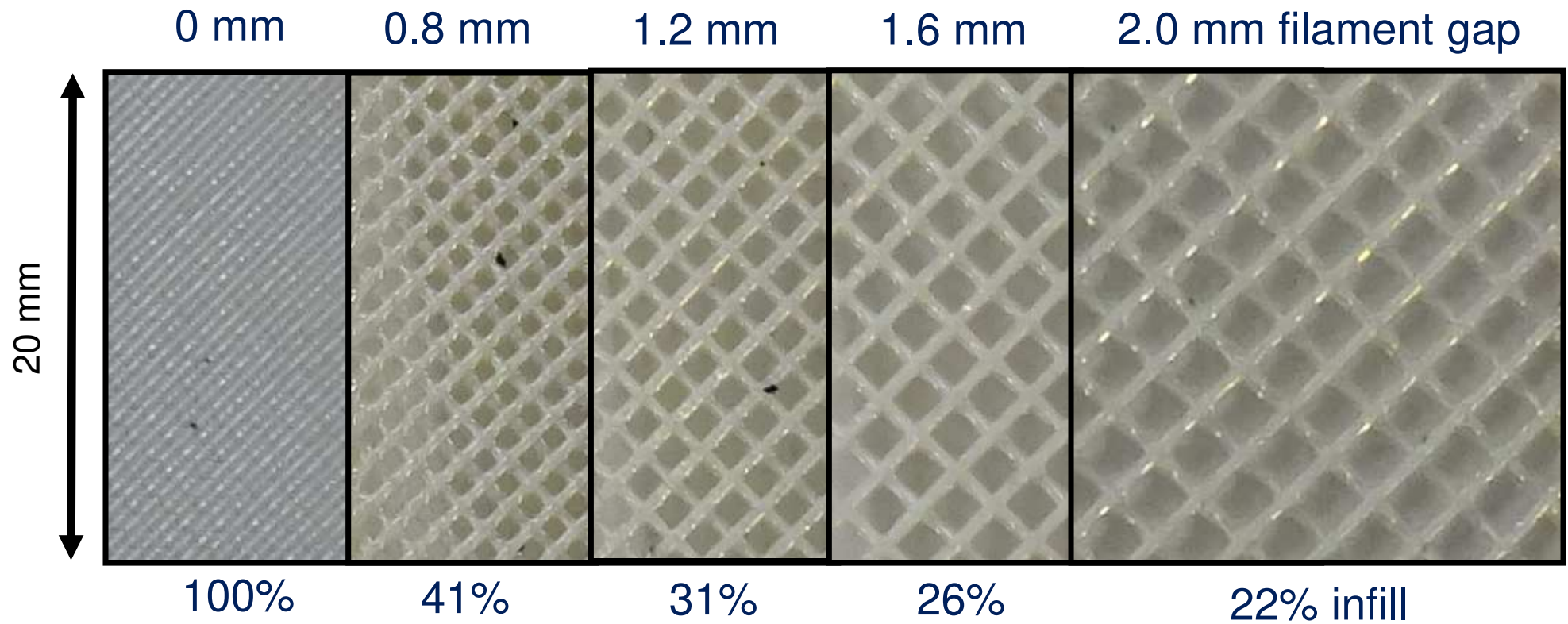


Parameter variation and test procedure: infill

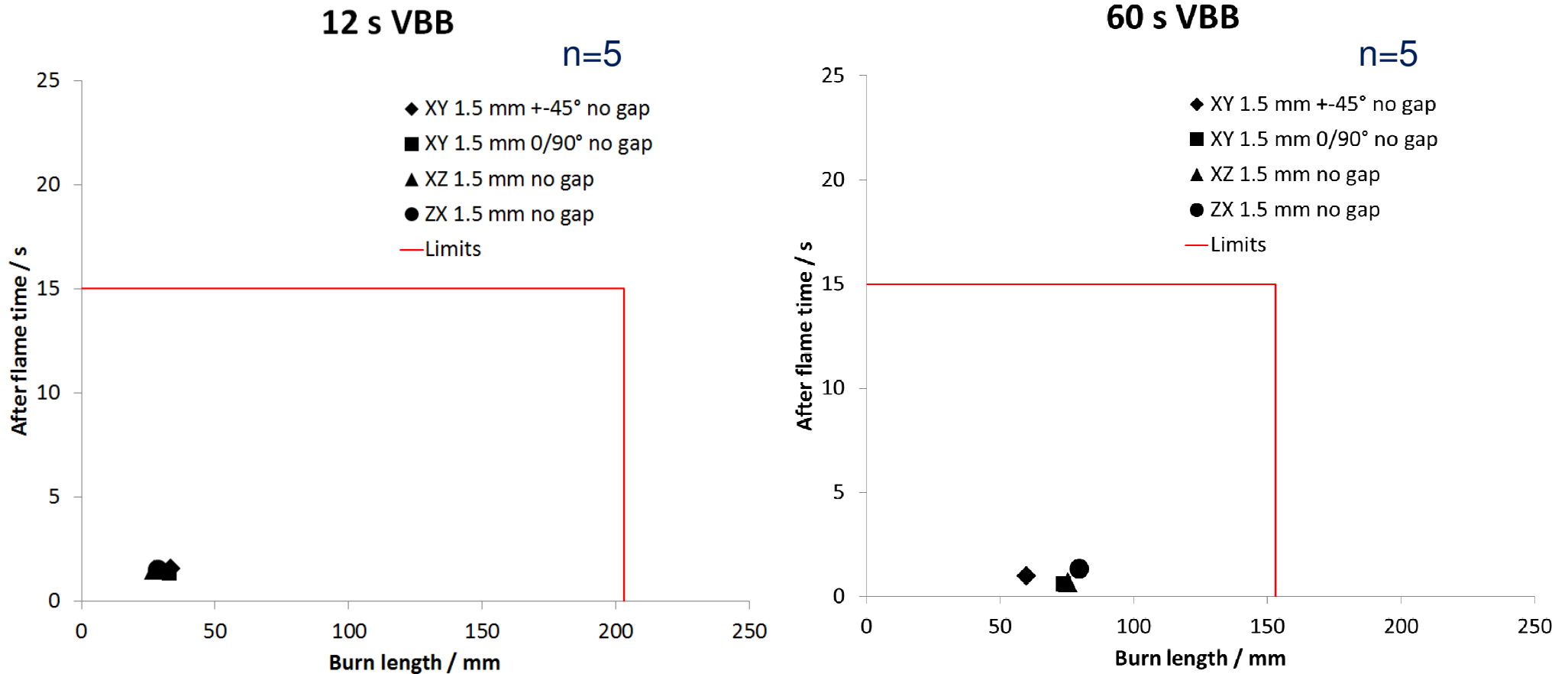


XZ and ZX: 1.5 mm too low to achieve a continuous open path → 2.0, 4.0 and 6.0 mm

Parameter variation and test procedure: infill



Results: 100% infill, influence of orientation

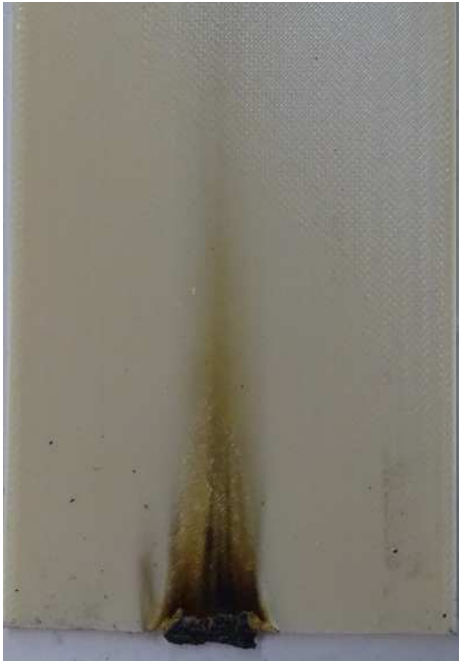


→ No influence of orientation for densest packing

Results: 100% infill, influence of orientation

12 s VBB

100 mm



XY $\pm 45^\circ$



XY 0/90°



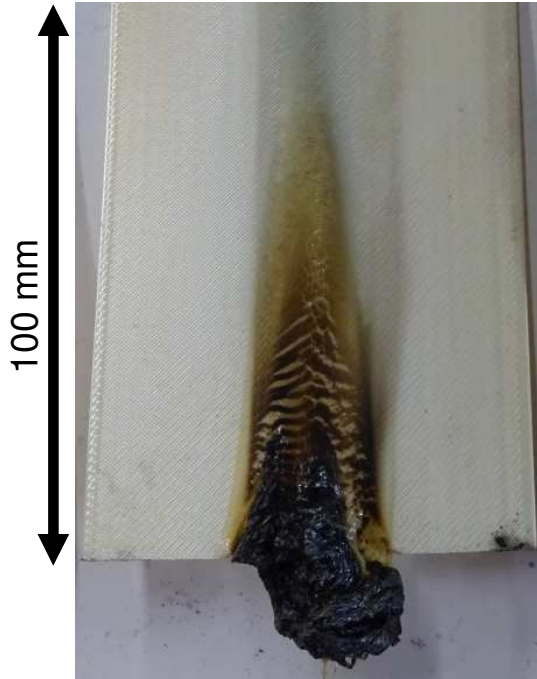
XZ



ZX

Results: 100% infill, influence of orientation

60 s VBB



XY $\pm 45^\circ$



XY 0/90°



XZ

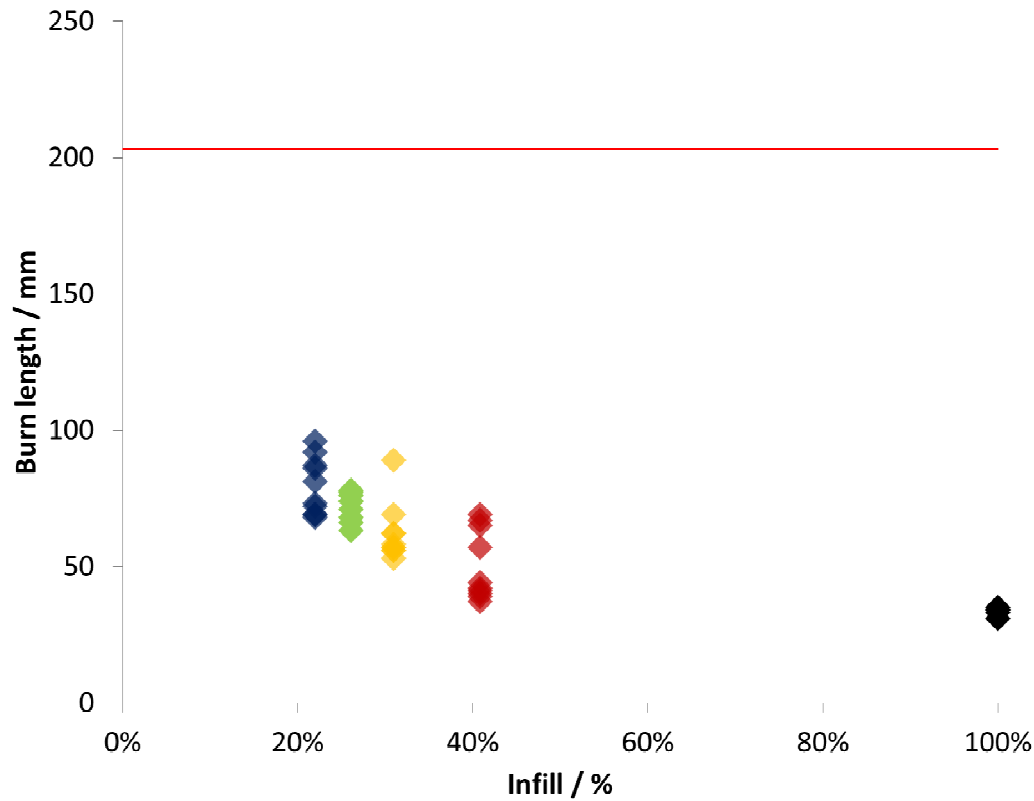


ZX

Results: XY $\pm 45^\circ$, variation of infill

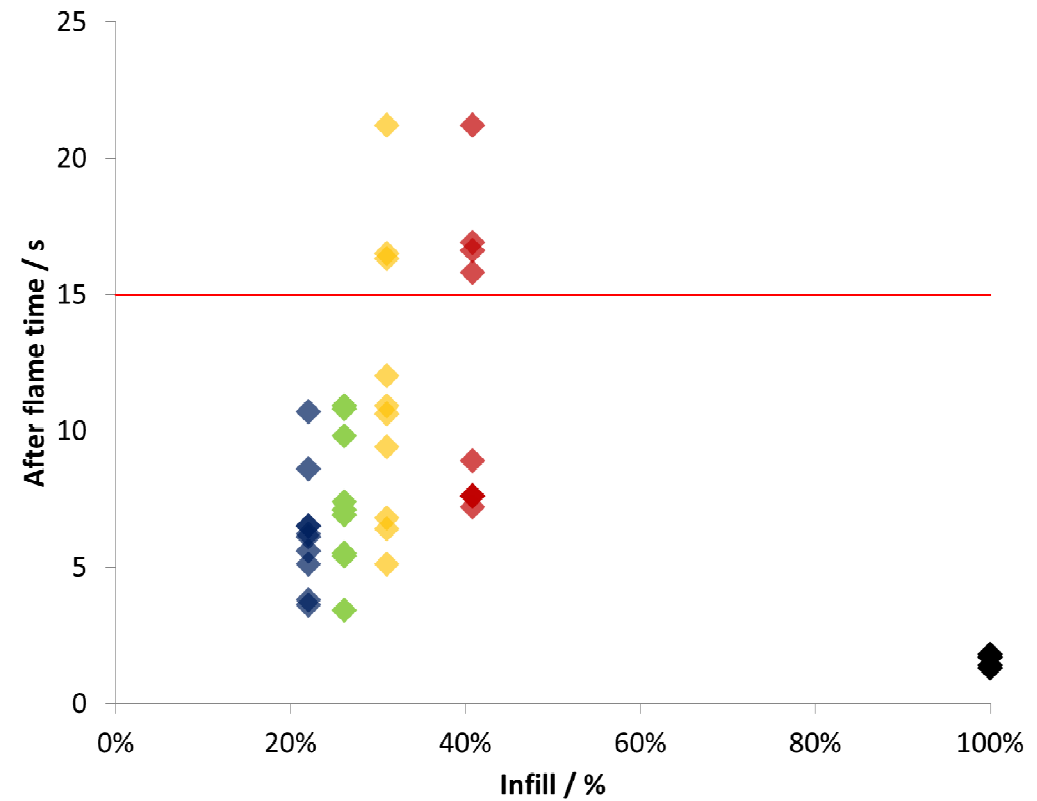
12 s VBB

n=10



12 s VBB

n=10

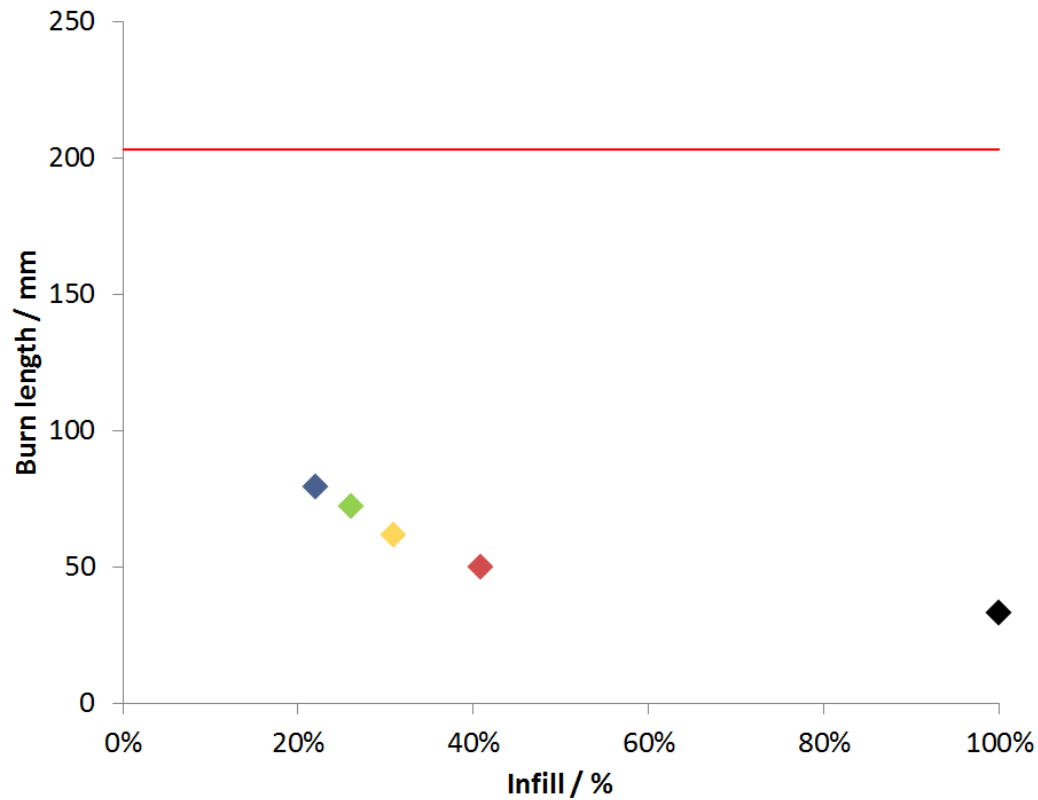


→ Lower infill = higher burn length and after flame

Results: XY $\pm 45^\circ$, variation of infill

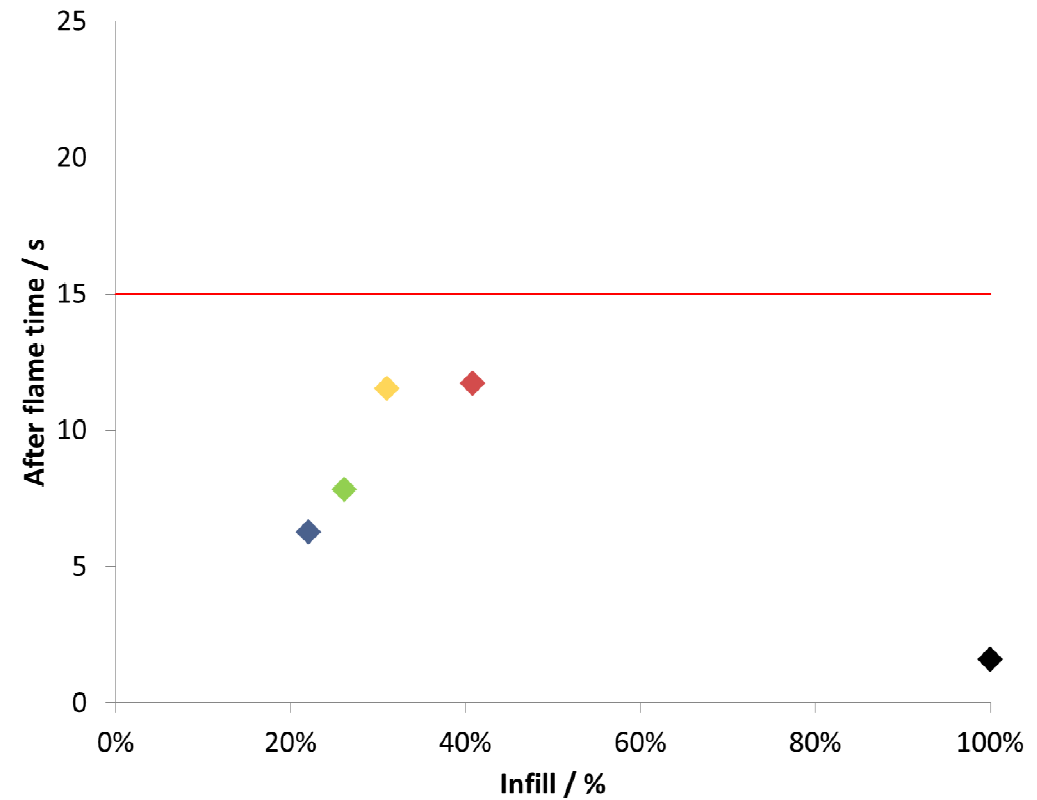
12 s VBB

n=10



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Results: $XY \pm 45^\circ$, variation of infill

12 s VBB

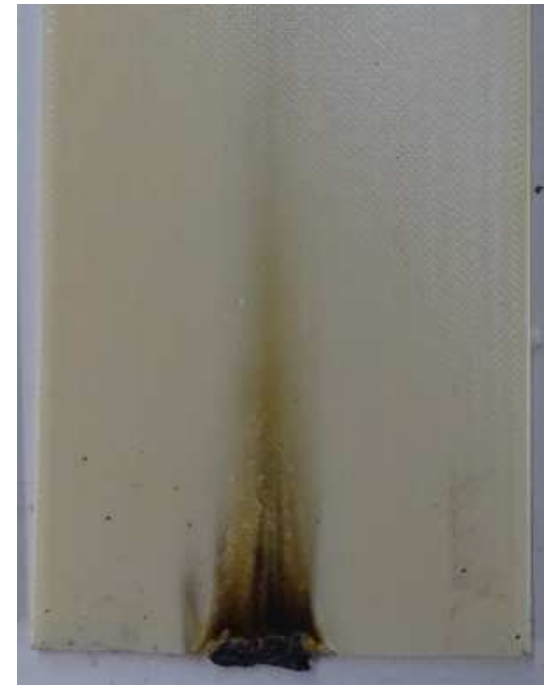
100 mm



22%



41%

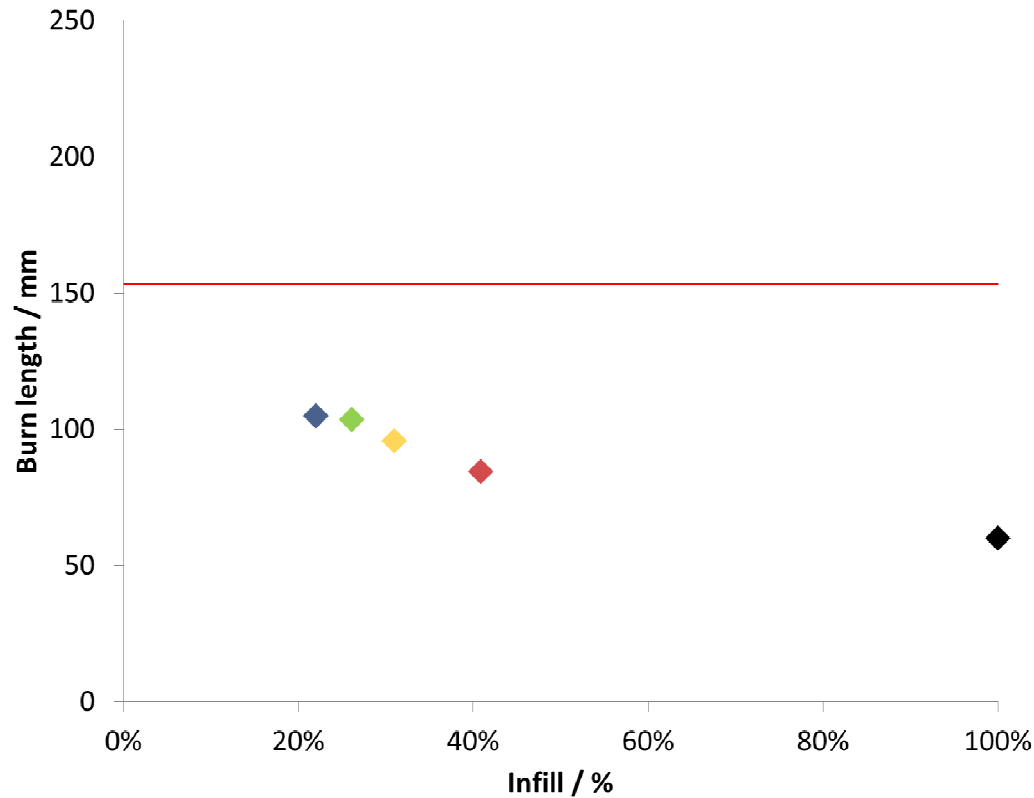


100%

Results: XY $\pm 45^\circ$, variation of infill

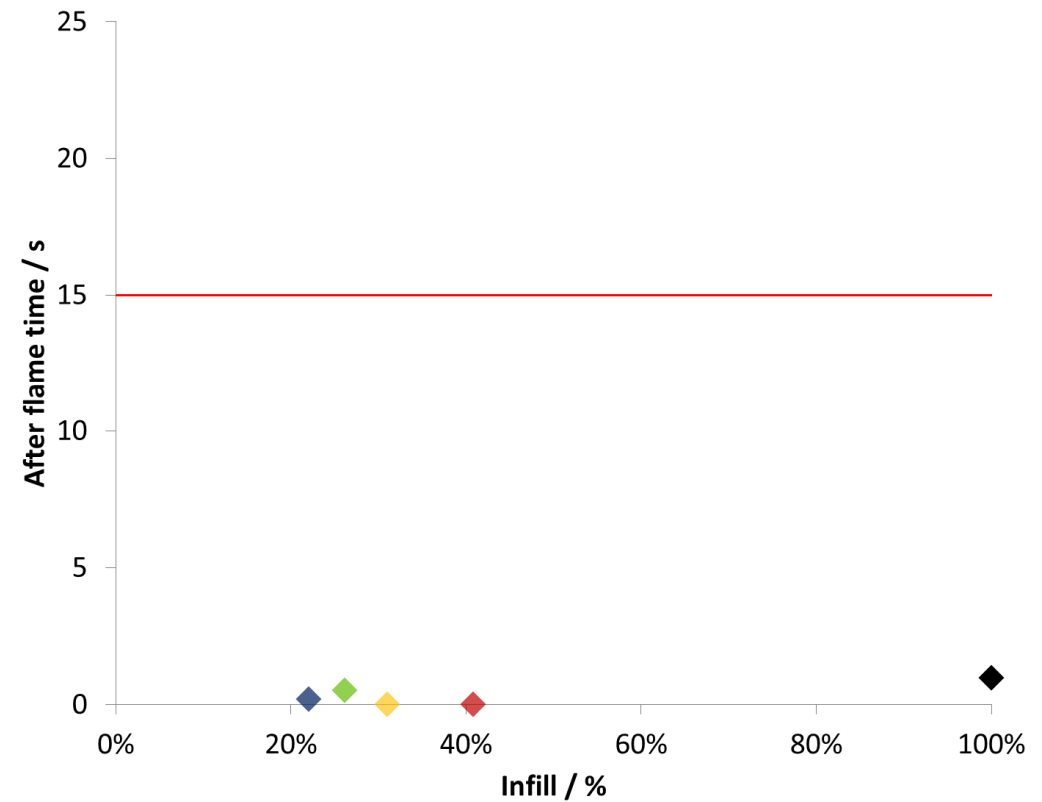
60 s VBB

n=10



60 s VBB

n=10



→ Lower infill = higher burn length

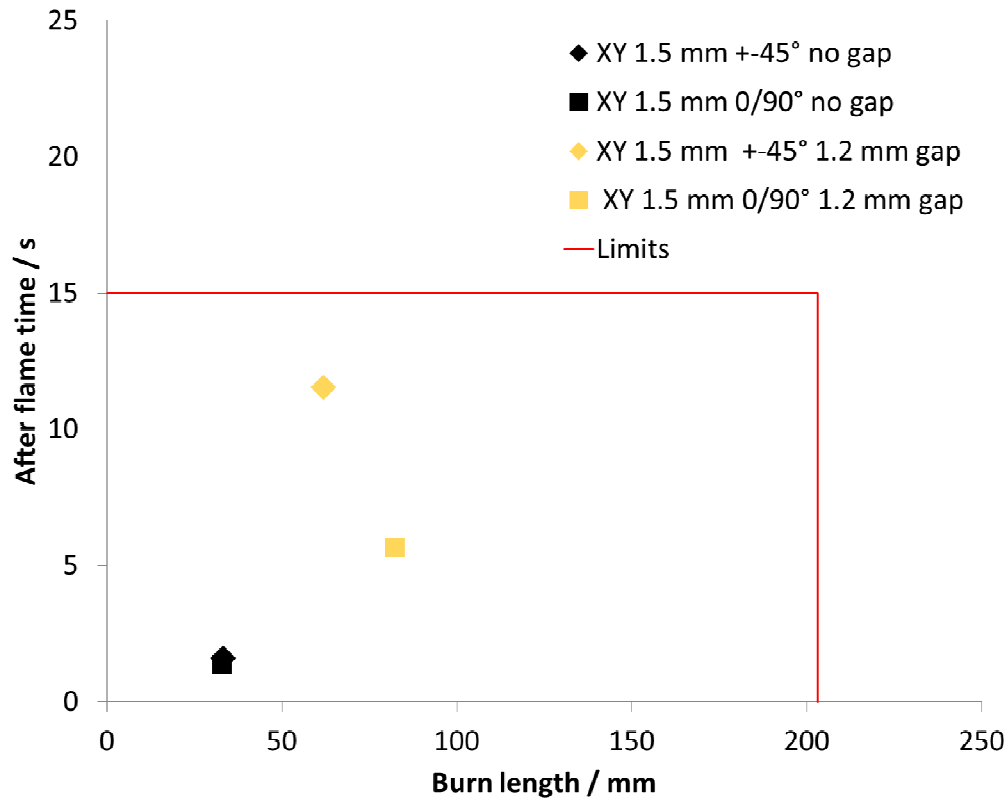
60 s 22% infill

0.000

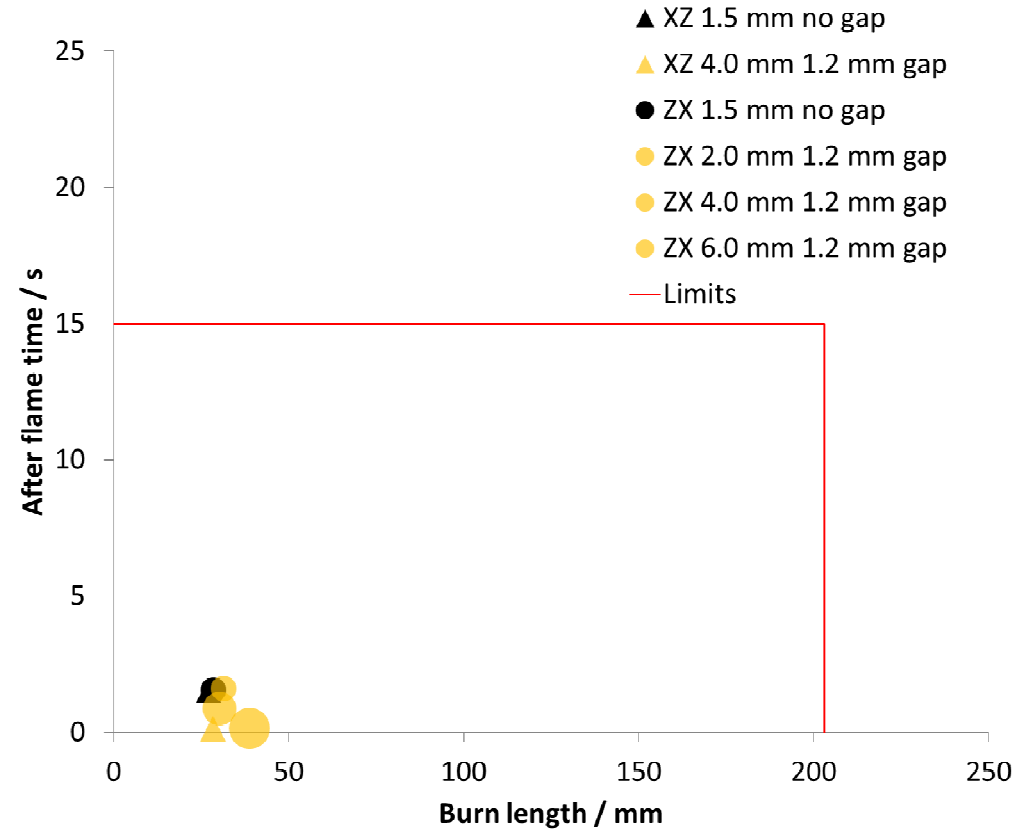
0.000

Results: variation of infill for different orientations

12 s VBB n=5-10

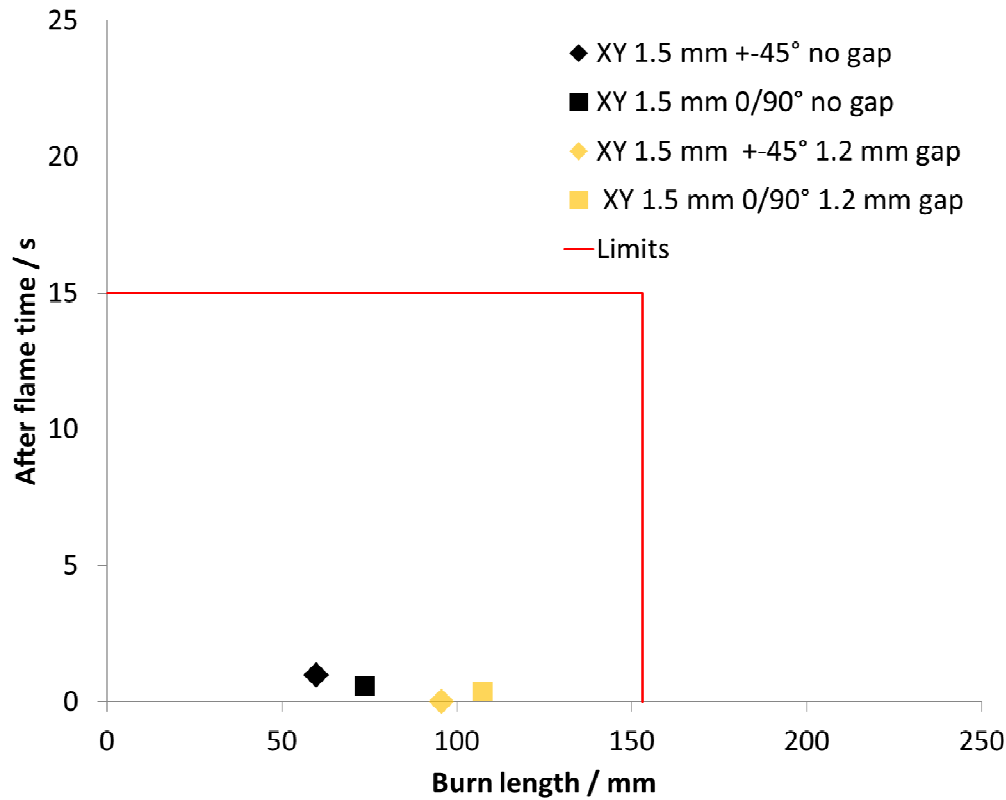


12 s VBB n=5-10

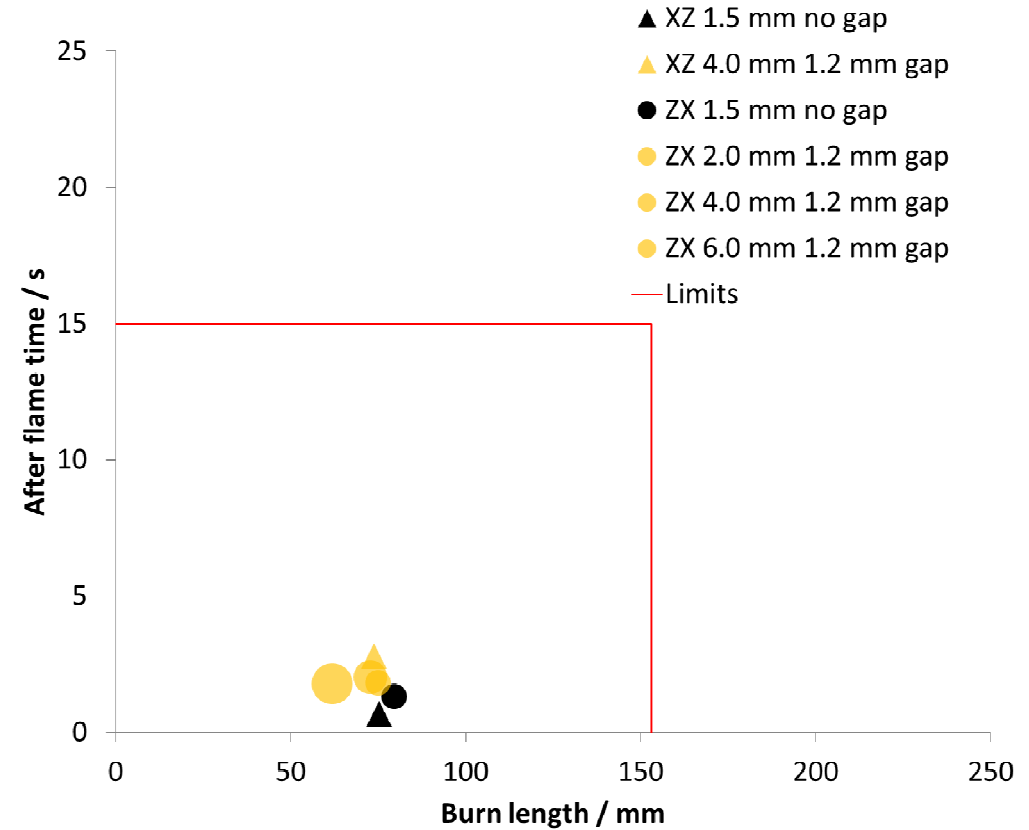


Results: variation of infill for different orientations

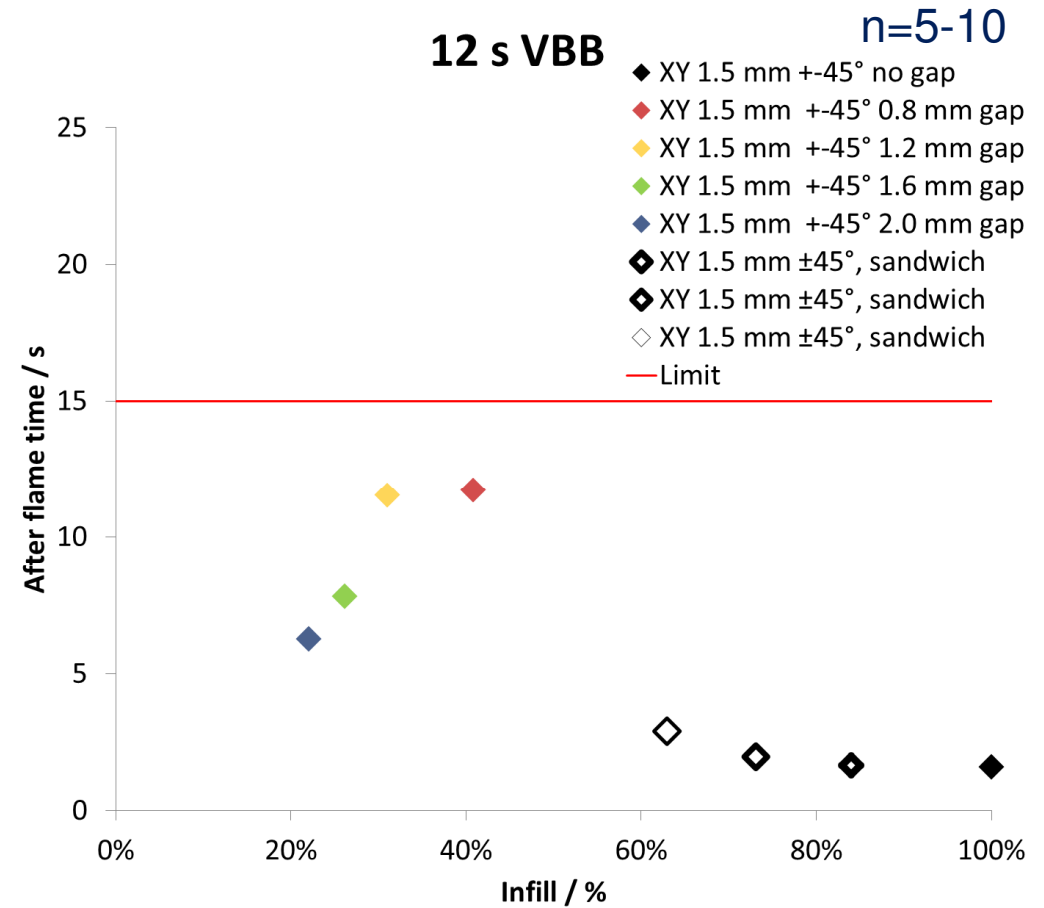
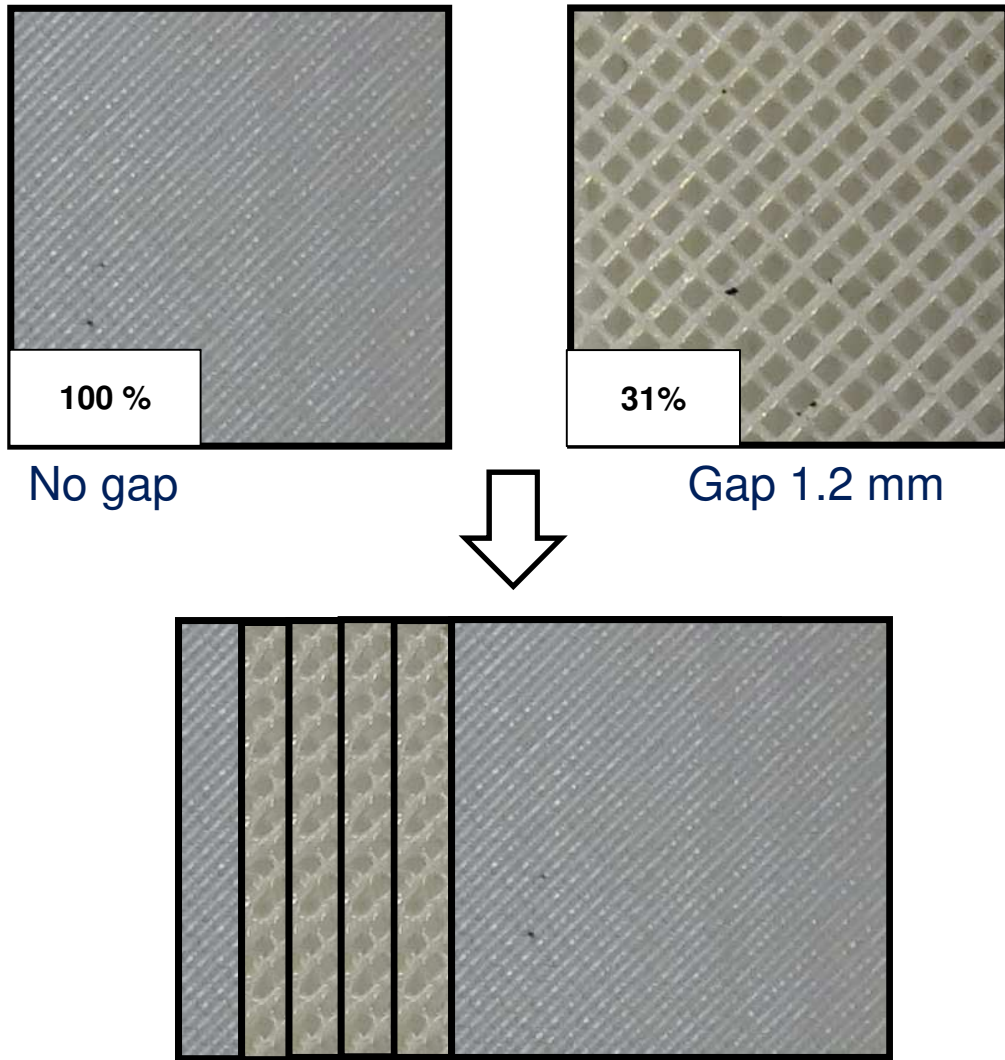
60 s VBB n=5-10



60 s VBB n=5-10

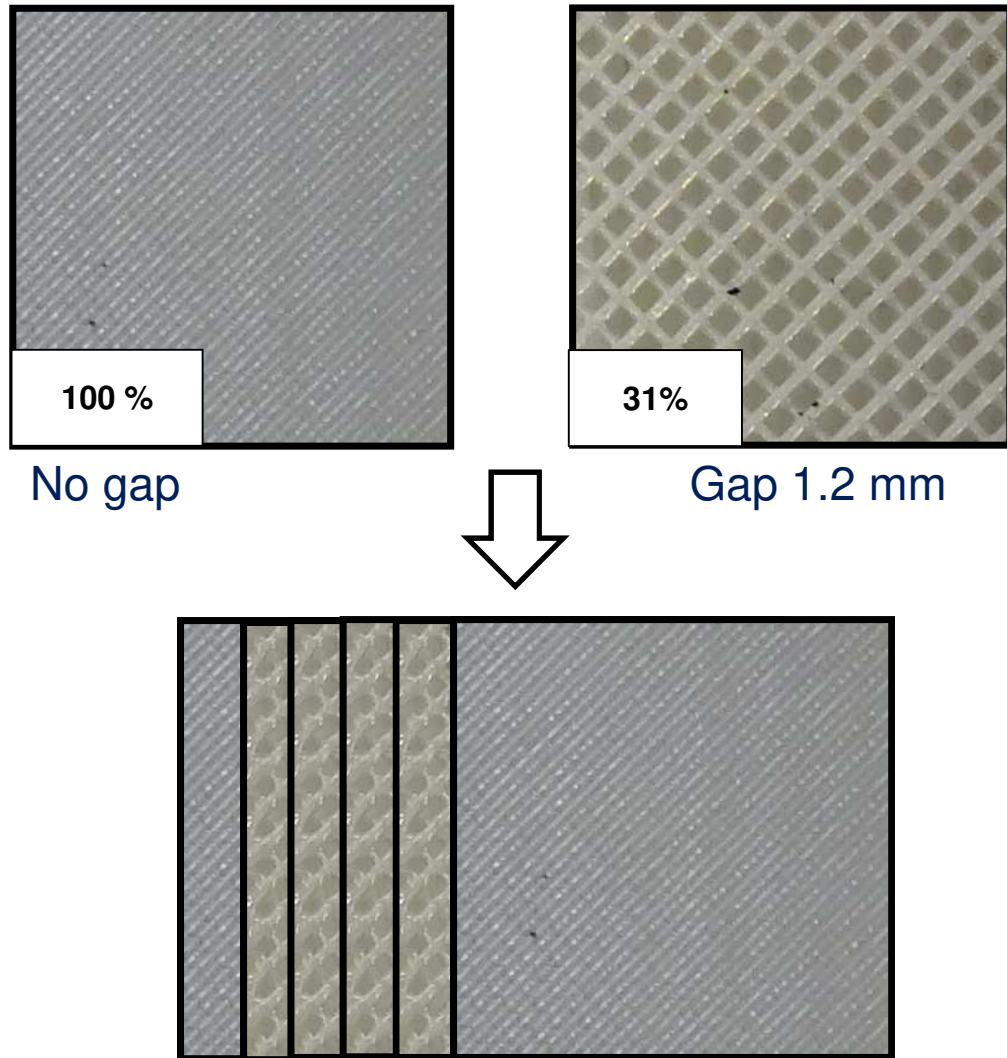


Results: sandwich coupons



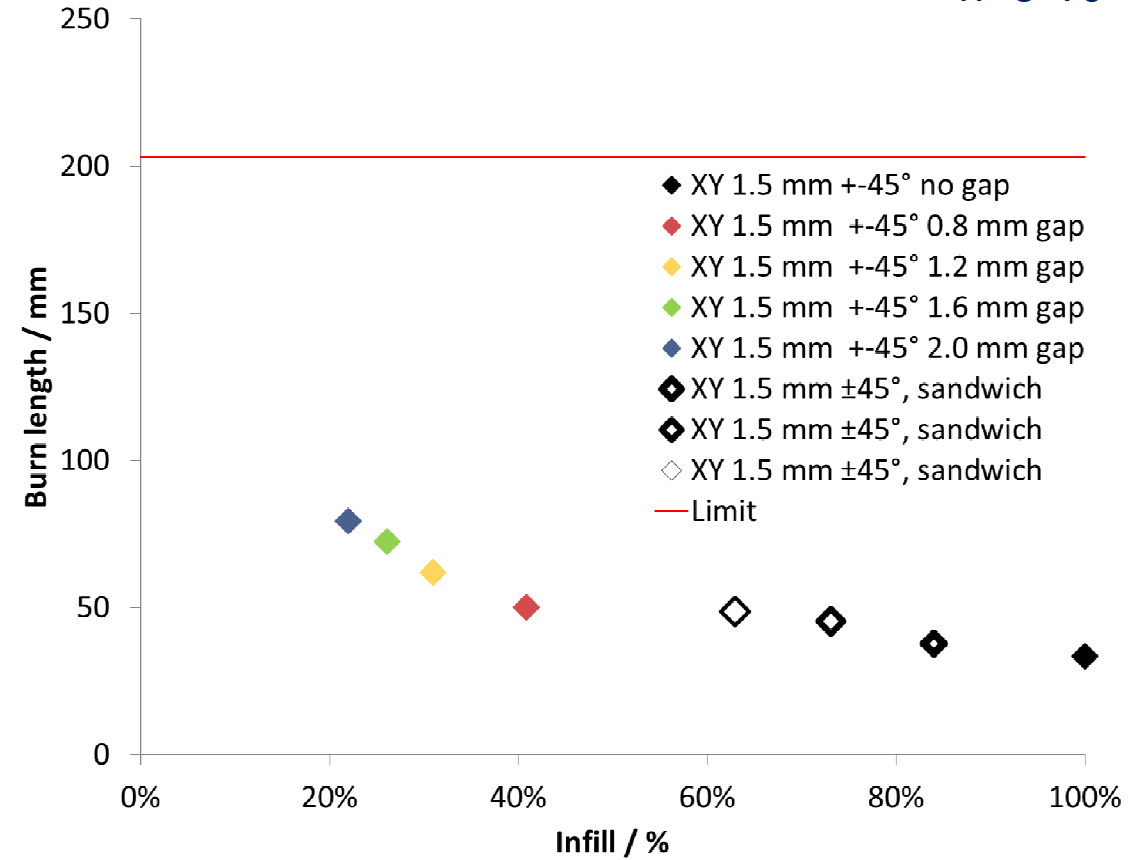
→ BL ~ infill, low influence on AF

Results: sandwich coupons



12 s VBB

n=5-10



→ BL ~ infill, low influence on AF

Results: sandwich coupons



63% XY $\pm 45^\circ$ sandwich



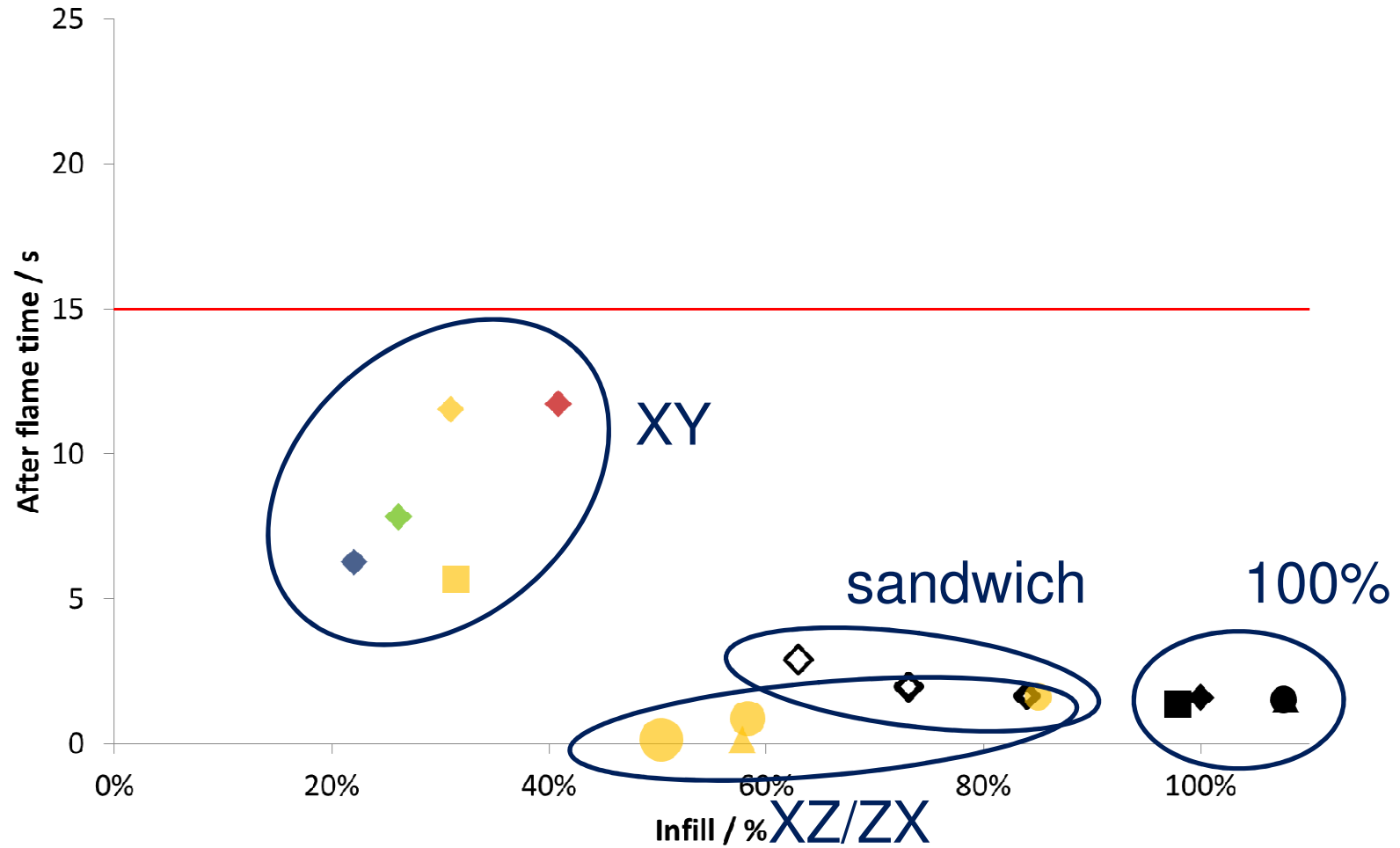
31 % XY $\pm 45^\circ$

→ Same burn length, but sandwich has shorter
after flame

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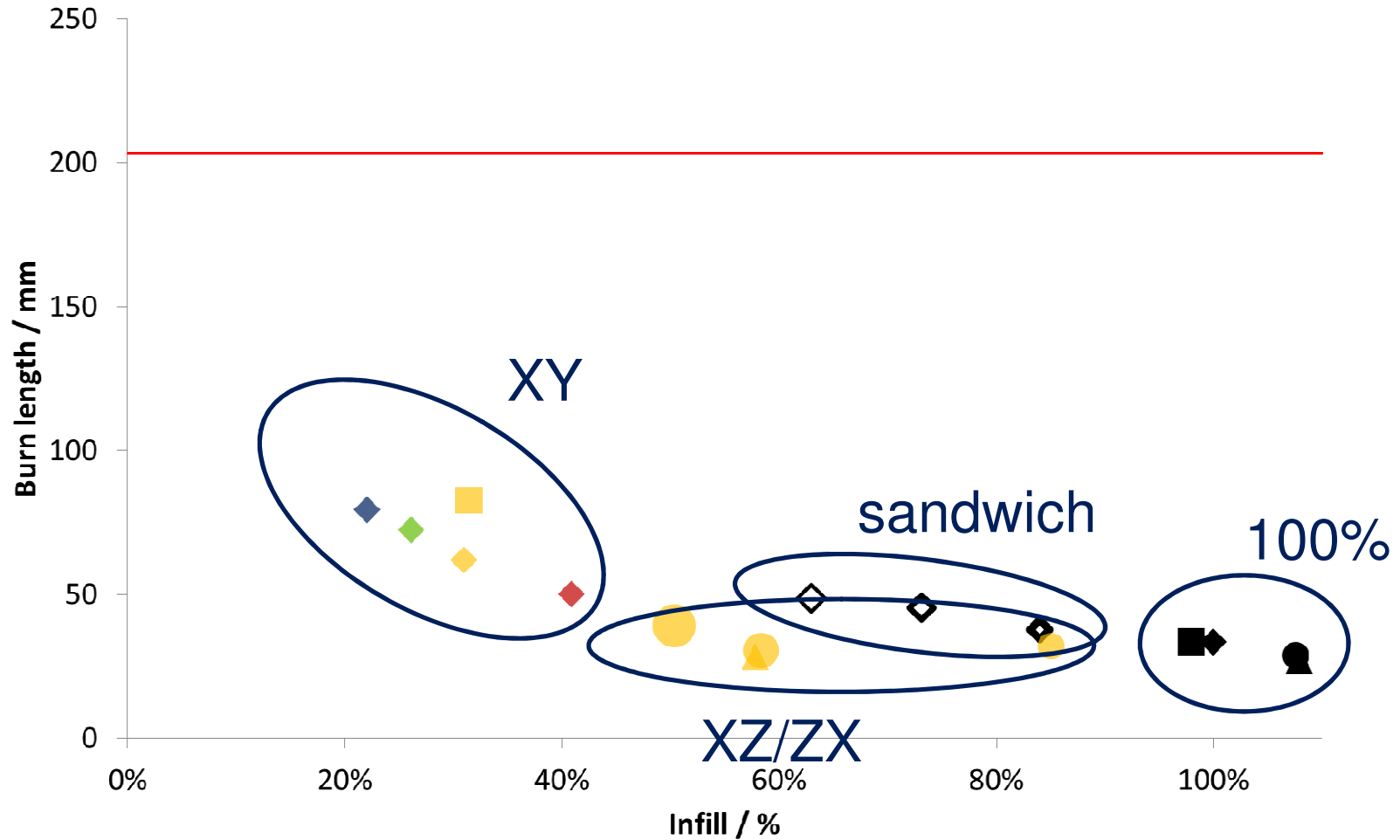
Results: Compilation

12 s VBB



Results: Compilation

12 s VBB

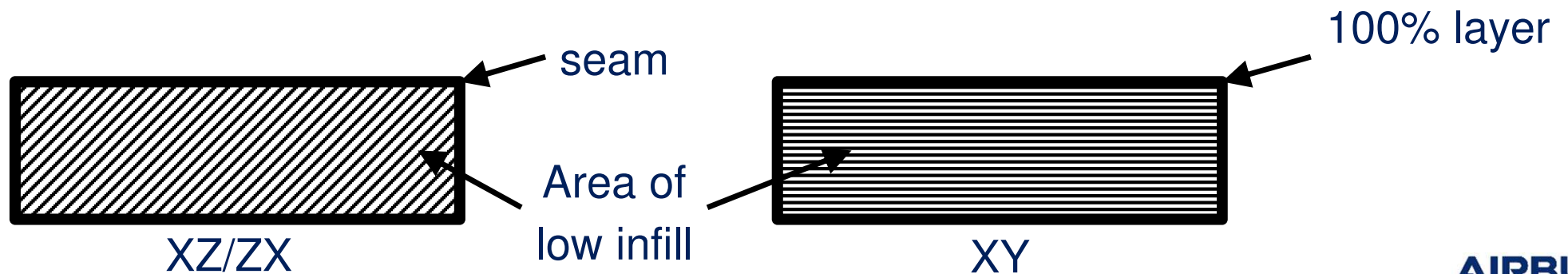


Discussion: Infill

- The pilot flame needs to warm up less material to the point of melting and gasification + air is present from all sides → combustion front can move quicker → higher burn length
- An after flame can stay lid longer due to the same reason. Cool down is prolonged, keeping the reaction intact for a longer time.

Discussion: orientation

- Densest packing leaves no room for particularities
- For lower infill, two types can be distinguished:
 1. Inside XY plane, behaviour is similar
 2. XZ and ZX resemble XY sandwich coupons in the cross section, hence results are similar



Discussion: DoE

- The number of different factors and their dependence or independence could be used in a DoE
- Expand data base for other materials printed via FDM

Infill	Gap size	Orientation	Thickness	Sandwich	Burn length	After flame
100%	0	XY $\pm 45^\circ$	1.5 mm	No		
⋮	1.2 mm	XY, 0/90°	2.0 mm	Yes		
⋮		XZ	4.0 mm			
⋮		ZX	6.0 mm			
22%						

Summary

- Thank you to Stratasyys & Airbus R&T for sponsoring the coupons!
- 12 s: Lower infill leads to (generally) higher burn length and after flame time
- 12 s: Orientation without influence for 100% infill
- 12 s: For sandwich configurations, burn length may be more dependent on the outer layer infill than after flame time
- 60 s: Shows low after flame times, burn length capped
- Go for further statistical analysis and other materials

Thank you

The Resorts Casino is older than the Tropicana.
How many years were in between their openings?



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3 1/2

